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UNIVERSITY OF CALIFORNIA PUBLICATIONS

IN

MATHEMATICS

Vol. 1, No. 7, pp. 163-169

February 16, 1915

QA1 C2 VII;7

ABRIDGED TABLES OF HYPERBOLIC FUNCTIONS

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BY

F. E. PERNOT

UNIVERSITY OF CALIFORNIA PRESS BERKELEY

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Cited as Univ. Calif. Publ. Math.

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MATHEMATICS

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ABRIDGED TABLES OF HYPERBOLIC FUNCTIONS.

BY

F. E. PERNOT

In the calculation of the operating characteristics of long transmission circuits the most convenient and direct solution is afforded by the use of hyperbolic functions of complex variables. For lines consisting of large conductors in which the losses are small it is desirable to make computations to the degree of accuracy afforded by six-place tables of logarithms. Also, in such cases, the argument to which the hyperbolic functions are taken from the tables is small; for power circuits usually below 0.5.

The most convenient table of these functions is that of the Smithsonian Institution, in which are tabulated both the logarithms and natural values for arguments from zero to 6.0, five decimal places being given. A table of Gudermannian functions is also appended, which makes it possible to find the values of functions (hyperbolic) to six places; not, however, without involving a double interpolation, first to the Gudermannian and then from a table of trigonometric functions.

For small arguments the hyperbolic cosine is not varying rapidly, hence easy interpolations are assured. The hyperbolic sine, on the other hand, is varying with the same rapidity as the argument, and therefore the interpolations for $\log \sinh x$ are cumbersome unless the tabular interval is very small. These considerations are immediately seen from the series expressing the two functions:

In all cases the hyperbolic tangent is most easily derived from $\sinh x$ and $\cosh x$ by

$$\tanh x = \frac{\sinh x}{\cosh x} \quad (2)$$

The series for $\sinh x$ in (1) can be written

$$\sinh x = x \left(1 + \frac{x^2}{|3|} + \frac{x^4}{|5|} + \frac{x^6}{|7|} + \dots \right)$$
 (3)

which immediately suggests the advisability of tabulating values of the quantity in brackets,

$$y = 1 + \frac{x^2}{3} + \frac{x^4}{5} + \frac{x^6}{7} + \dots$$
 (4)

for this quantity is seen to have an even smaller rate of change than $\cosh x$. The value of the hyperbolic sine is then given by

$$\begin{array}{c}
\sinh x = xy \\
y = \frac{\sinh x}{x}
\end{array} \right\} (5)$$

Since extended computations are most conveniently done by logarithms, the tabulation was made of $\log y$. Log x naturally being at hand, the value of $\log \sinh x$ is immediately found by simple addition of $\log x$ and $\log y$, and, further, it is found without having to make any inconvenient interpolations. A glance at the values of $\log \sinh x$ as tabulated in any table will immediately impress one with the impracticability of interpolating directly for $\log \sinh x$ for values of x between 0 and 0.10, in which region a large proportion of the values of x fall for the particular work above referred to. This scheme of tabulating the ratio of a function of a variable to the variable itself is the same as is used in the "S and T" tables found in Bremiker's logarithm tables, where for small angles the ratios of the trigonometric sine and tangent to the angle are given.

CONSTRUCTION OF TABLES

The following table contains values to base 10 of $\log \frac{\sinh x}{x}$ and $\log \cosh x$, together with the differences to be used in interpolating. The arguments progress in steps of 0.005 from zero to 0.600, giving 121 entries. Logarithms are given to seven places.

The first column, $\log_{10} \frac{\sinh x}{x}$, was computed by first evaluating the expression for y in (4) and then taking out $\log y$ from tables. For the small values of x

used, this series is very convergent, hence the labor involved was not excessive. The evaluation of the series was made for alternate entries, and the intermediate values obtained by interpolation.

Using this value of $\log \frac{\sinh x}{x}$ the value of $\log \frac{1}{\sinh^2 x}$ was formed. Using this

as argument in Zech's table of addition logarithms, the value of $\log_{10} \cosh^2 x$ is immediately obtained, from the relation $\cosh^2 x = \sinh^2 x + 1$. Interpolations in the addition logarithm tables were made to the nearest even number in order that the resulting value of $\log \cosh x$ might appear to the nearest unit in the last place.

The complete set of values was checked by differences, and in a few cases the last unit was changed by one in order to give uniformity in the second differences, which in both tabulations are practically constant.

In addition to the check by differences, every tenth entry was checked independently by calculating directly the values of

$$y = \frac{\sinh x}{x} = \frac{\epsilon^x - \epsilon^{-x}}{2x}$$
 and $\cosh x = \frac{\epsilon^x + \epsilon^{-x}}{2}$,

using the tabulated values of the exponentials as given to nine decimals in tables of the exponential function by J. W. L. Glaisher, F. R. S., published in the *Transactions of the Cambridge Philosophical Society*, vol. XIII. From the above values, the logarithm to seven places was taken from tables, which agreed with the previously tabulated values to the nearest unit of the last place, except in two or three cases where a difference of one was noted.

To facilitate interpolation, the values of the first derivatives of the function multiplied by the tabular interval ($\omega = 0.005$) are tabulated in units of the last place in the tabulated seven-place logarithm of the function. The second differences are also tabulated.

For the first three columns:

$$f(x) = \log_{10} \frac{\sinh x}{x} = \log_{10} y$$

$$\omega f'(x) = \omega \frac{d}{dx} \log_{10} \frac{\sinh x}{x} = \omega \frac{d}{dx} \log_{10} y$$

$$= \omega \frac{d}{dx} \log_{10} (1 + \frac{x^{2}}{\underline{13}} + \frac{x^{4}}{\underline{15}} + \dots)$$

$$= 2\omega M \frac{x}{y} \left(\frac{1}{\underline{13}} + \frac{2x^{2}}{\underline{15}} + \frac{3x^{4}}{\underline{17}} + \frac{4x^{6}}{\underline{19}} + \dots \right)$$
(6)

M = modulus of the common logarithm system = 0.43429448.

This series is very convergent, and was used in the form for the value of $\omega = 0.005$,

$$\omega f'(x) = 0.01M \frac{x}{y} \left(\frac{1}{\underline{3}} + \frac{2x^2}{\underline{5}} + \frac{3x^4}{\underline{7}} + \dots \right)$$
 (7)

Of course the above value was multiplied by 10^7 to reduce to units of the last place in the tabulation of log y. Values of log y to be used in the computation were taken directly from the table.

 Δ_2 is the average of the differences in $\omega f'(x)$ immediately preceding and following a tabular value of log y.

For the last three columns:

$$f(x) = \log_{10} \cosh x$$

$$\omega f'(x) = \omega \frac{d}{dx} \log_{10} \cosh x$$

$$= \omega M \frac{\sinh x}{\cosh x}$$
(8)

Thus

$$\omega f'(x) = 0.005M \tanh x \quad (9)$$

 Δ_2 is the same as defined for the previous case.

It is to be noted that the second differences, or accelerations if x be considered equicrescent, are practically constant. Easy and accurate interpolations are thus assured, even to seven decimals and for tabular intervals in the argument as great as 0.005, which is five times as great an interval as is used in the Smithsonian Tables for the functions tabulated to five decimals only.

TO INTERPOLATE USING SECOND DIFFERENCES

Let it be required to determine the value of f(x) for an argument

$$x = x_0 \pm a$$

 x_0 is the value of the argument nearest that of x. a, then, is the distance over which the interpolation has to be made, and $\frac{a}{\omega} = n =$ the fraction of the tabular interval. Using the second differences, we have

$$f(x) = f(x_0 \pm n\omega) = f(x_0) \pm n \, \omega f'(x) + \frac{n^2}{2} \Delta_2$$
 (10)

 $f(x_0)$ is the value of the function corresponding to the argument x_0 .

Illustration:

Required,
$$\log \sinh 0.1163740$$

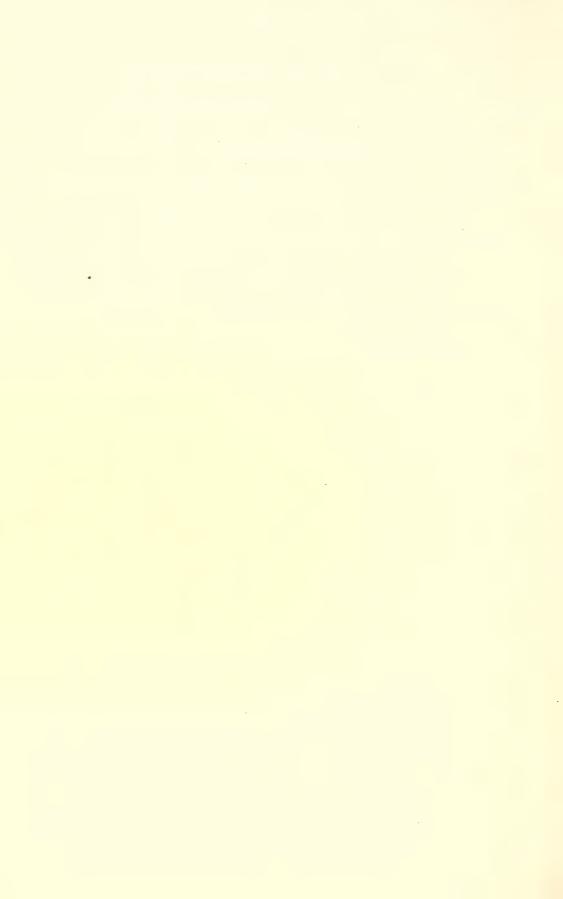
 $\log \cosh 0.1163740$
 $x = 0.1163740$
 $x_0 = 0.115$
 $a = +0.0013740$
 $n = \frac{a}{.005} = +0.27480$

LOGARITHMS OF HYPERBOLIC FUNCTIONS OF A REAL VARIABLE From x=0 to x=0.600

| x | $\log_{10} \frac{\sinh x}{x}$ | $\omega f'(x)$ | Δ_2 | $\log_{10} \cosh x$ | $\omega f'(x)$ | Δ_2 |
|-------|-------------------------------|----------------|------------|---------------------|----------------|---------------|
| 0.000 | 0.00000000 | 0.000 | 36.2 | 0.0000000 | 0.000 | 108.6 |
| .005 | .0000018 | 36.2 | 36.2 | .0000054 | 108.6 | 108.6 |
| .010 | .0000072 | 72.4 | 36.2 | .0000217 | 217.1 | 108.6 |
| .015 | .0000162 | 108.6 | 36.2 | .0000489 | 325.7 | 108.6 |
| .020 | .0000289 | 144.8 | 36.2 | .0000869 | 434.2 | 108.5 |
| | | | | | 101,2 | 100.0 |
| .025 | .0000452 | 180.9 | 36.2 | .0001357 | 542.8 | 108.5 |
| .030 | .0000651 | 217.1 | 36.2 | .0001954 | 651.2 | 108.5 |
| .035 | .0000886 | 253.3 | 36.2 | .0002659 | 759.7 | 108.4 |
| .040 | .0001158 | 289.5 | 36.2 | .0003473 | 868.1 | 108.4 |
| .045 | .0001466 | 325.7 | 36.2 | .0004396 | 976.5 | 108.4 |
| | | | | | | |
| .050 | .0001809 | 361.8 | 36.2 | .0005426 | 1084.8 | 108.3 |
| .055 | .0002189 | 398.0 | 36.2 | .0006565 | 1193.1 | 108.2 |
| .060 | .0002605 | 434.2 | 36.2 | .0007813 | 1301.3 | 108.2 |
| .065 | .0003057 | 470.4 | 36.2 | .0009168 | 1409.5 | 108.1 |
| .070 | .0003546 | 506.5 | 36.2 | .0010632 | 1517.5 | 108.0 |
| .075 | 0004071 | 540 F | 0.0.0 | | | |
| .080 | .0004071 | 542.7 | 36.2 | .0012203 | 1625.6 | 108.0 |
| .085 | .0004632 $.0005229$ | 578.8 | 36.1 | .0013882 | 1733.5 | 107.9 |
| .090 | | 615.0 | 36.1 | .0015670 | 1841.3 | 107.8 |
| .095 | .0005862 | 651.1 | 36.1 | .0017565 | 1949.1 | 107.7 |
| .095 | .0006531 | 687.2 | 36.1 | .0019568 | 2056.7 | 107.6 |
| .100 | .0007236 | 723.3 | 36.1 | .0021679 | 2164.3 | 107.5 |
| .105 | .0007977 | 759.4 | 36.1 | .0023897 | 2271.7 | 107.4 |
| .110 | .0008755 | 795.6 | 36.1 | .0026222 | 2379.0 | 107.3 |
| .115 | .0009569 | 831.7 | 36.1 | .0028655 | 2486.2 | 107.2 |
| .120 | .0010418 | 867.8 | 36.1 | .0031194 | 2593.3 | 107.0 |
| | | | | | | |
| .125 | .0011304 | 903.8 | 36.1 | .0033841 | 2700.3 | 106.9 |
| .130 | .0012226 | 939.9 | 36.1 | .0036595 | 2807.1 | 106.8 |
| .135 | .0013184 | 976.0 | 36.0 | .0039456 | 2913.8 | 106.6 |
| .140 | .0014178 | 1012.0 | 36.0 | .0042423 | 3020.4 | 106.5 |
| .145 | .0015208 | 1048.1 | 36.0 | .0045496 | 3126.8 | 106.3 |
| 4 80 | | | | | | |
| .150 | .0016274 | 1084.1 | 36.0 | .0048676 | 3233.0 | 106.2 |
| .155 | .0017376 | 1120.1 | 36.0 | .0051962 | 3339.1 | 106.0 |
| .160 | .0018514 | 1156.1 | 36.0 | .0055354 | 3445.0 | 105.8 |
| .165 | .0019688 | 1192.1 | 36.0 | .0058852 | 3550.8 | 105.7 |
| .170 | .0020899 | 1228.1 | 36.0 | .0062456 | 3656.3 | 105.5 |
| .175 | .0022145 | 1264.1 | 36.0 | .0066165 | 3761.8 | 105.3 |
| .180 | .0023427 | 1300.1 | 36.0 | .0069979 | 3867.0 | 105.3 |
| .185 | .0024745 | 1336.0 | 36.0 | .0073899 | 3972.0 | 104.9 |
| .190 | .0026099 | 1372.0 | 36.0 | .0077923 | 4076.9 | 104.9 104.7 |
| .195 | .0027489 | 1407.9 | 35.9 | .0082052 | 4181.5 | 104.7 |
| | | | 00,0 | .0002002 | 1101.0 | 104.0 |
| .200 | .0028915 | 1443.8 | 35.9 | .0086286 | 4286.0 | 104.3 |
| | | | | | | |

| | ainh a | | | | | |
|------|-------------------------------|----------------|------------|--------------------|----------------|------------|
| x | $\log_{10} \frac{\sinh x}{x}$ | $\omega f'(x)$ | Δ_2 | $\log_{10}\cosh x$ | $\omega f'(x)$ | Δ_2 |
| .200 | .0028915 | 1443.8 | 35.9 | .0086286 | 4286.0 | 104.3 |
| .205 | .0030377 | 1479.7 | 35.9 | .0090624 | 4390.2 | 104.1 |
| .210 | .0031874 | 1515.6 | 35.9 | .0095066 | 4494.2 | 103.9 |
| .215 | .0033407 | 1551.4 | 35.9 | .0099612 | 4598.0 | 103.7 |
| .220 | .0034977 | 1587.3 | 35.8 | .0104262 | 4701.6 | 103.5 |
| .225 | .0036582 | 1623.1 | 35.8 | .0109015 | 4805.0 | 103.3 |
| .230 | .0038223 | 1658.9 | 35.8 | .0113872 | 4908.1 | 103.0 |
| .235 | .0039900 | 1694.7 | 35.8 | .0118832 | 5011.1 | 102.8 |
| .240 | .0041612 | 1730.5 | 35.8 | .0123894 | 5113.7 | 102.5 |
| .245 | .0043361 | 1766.3 | 35.8 | .0129059 | 5216.2 | 102.3 |
| .250 | .0045145 | 1802.1 | 35.7 | .0134326 | 5318.3 | 102.1 |
| .255 | .0046965 | 1837.8 | 35.7 | .0139696 | 5420.3 | 101.8 |
| .260 | .0048821 | 1873.5 | 35.7 | .0145167 | 5522.0 | 101.6 |
| .265 | .0050712 | 1909.2 | 35.7 | .0150739 | 5623.4 | 101.3 |
| .270 | .0052639 | 1944.9 | 35.7 | .0156413 | 5724.5 | 101.0 |
| .275 | .0054602 | 1980.5 | 35.6 | .0162188 | 5825.4 | 100.8 |
| .280 | .0056600 | 2016.2 | 35.6 | .0168064 | 5926.1 | 100.5 |
| .285 | .0058634 | 2051.8 | 35.6 | .0174040 | 6026.4 | 100.2 |
| .290 | .0060704 | 2087.4 | 35.6 | .0180117 | 6126.5 | 99.9 |
| .295 | .0062809 | 2123.0 | 35.6 | .0186293 | 6226.3 | 99.7 |
| .300 | .0064950 | 2158.5 | 35.5 | .0192569 | 6325.8 | 99.4 |
| .305 | .0067126 | 2194.0 | 35.5 | .0198945 | 6425.0 | 99.1 |
| .310 | .0069338 | 2229.6 | 35.5 | .0205419 | 6523.9 | 98.8 |
| .315 | .0071586 | 2265.1 | 35.5 | .0211993 | 6622.5 | 98.5 |
| .320 | .0073869 | 2300.6 | 35.5 | .0218665 | 6720.9 | 98.2 |
| .325 | .0076187 | 2336.0 | 35.4 | .0225435 | 6818.9 | 97.9 |
| .330 | .0078541 | 2371.5 | 35.4 | .0232302 | 6916.6 | 97.6 |
| .335 | .0080930 | 2406.9 | 35.4 | .0239267 | 7014.0 | 97.2 |
| .340 | .0083354 | 2442.2 | 35.4 | .0246330 | 7111.1 | 96.9 |
| .345 | .0085814 | 2477.6 | 35.3 | .0253490 | 7207.8 | 96.6 |
| .350 | .0088309 | 2512.9 | 35.3 | .0260746 | 7304.3 | 96.3 |
| .355 | .0090839 | 2548.2 | 35.3 | .0268098 | 7400.4 | 96.0 |
| .360 | .0093405 | 2583.5 | 35.3 | .0275546 | 7496.2 | 95.6 |
| .365 | .0096006 | 2618.8 | 35.2 | .0283090 | 7591.7 | 95.3 |
| .370 | .0098643 | 2654.0 | 35.2 | .0290730 | 7686.8 | 95.0 |
| .375 | .0101315 | 2689.2 | 35.2 | .0298464 | 7781.6 | 94.6 |
| .380 | .0104022 | 2724.4 | 35.2 | .0306293 | 7876.1 | 94.3 |
| .385 | .0106764 | 2759.5 | 35.1 | .0314216 | 7970.2 | 93.9 |
| .390 | .0109541 | 2794.7 | 35.1 | .0322233 | 8064.0 | 93.6 |
| .395 | .0112353 | 2829.8 | 35.1 | .0330344 | 8157.4 | 93.3 |
| .400 | .0115201 | 2864.9 | 35.1 | .0338548 | 8250.5 | 92.9 |
| .405 | .0118083 | 2899.9 | 35.0 | .0346845 | 8343.2 | 92.6 |
| .410 | .0121000 | 2934.9 | 35.0 | .0355234 | 8435.6 | 92.2 |
| .415 | .0123952 | 2969.9 | 35.0 | .0363716 | 8527.6 | 91.8 |
| .420 | .0126940 | 3004.9 | 35.0 | .0372289 | 8619.2 | 91.5 |
| .425 | 0.0129963 | 3039.8 | 34.9 | .0380954 | 8710.5 | 91.1 |

| x | $\log_{10} \frac{\sinh x}{x}$ | $\omega f'(x)$ | Δ_2 | $\log_{10} \cosh x$ | $\omega f'(x)$ | Δ_2 |
|------|-------------------------------|----------------|------------|---------------------|----------------------|------------|
| .425 | 0.0129963 | 3039.8 | 34.9 | .0380954 | 8710.5 | 91.1 |
| .430 | .0133020 | 3074.7 | 34.9 | .0389710 | 8801.4 | 90.7 |
| .435 | .0136112 | 3109.6 | 34.9 | .0398557 | 8892.0 | 90.4 |
| .440 | .0139239 | 3144.5 | 34.8 | .0407494 | 8982.2 | 90.0 |
| .445 | 0.142400 | 3179.3 | 34.8 | .0416521 | 9072.0 | 89.6 |
| .450 | .0145597 | 3214.1 | 34.8 | .0425638 | 9161.4 | 89.3 |
| .455 | .0148828 | 3248.8 | 34.7 | .0434844 | 9250.5 | 88.9 |
| .460 | .0152095 | 3283.5 | 34.7 | .0444139 | 9339.2 | 88.5 |
| .465 | .0155396 | 3318.2 | 34.7 | .0453522 | 9427.5 | 88.1 |
| .470 | .0158732 | 3352.9 | 34.6 | .0462993 | 9515.4 | 87.7 |
| .475 | .0162102 | 3387.5 | 34.6 | .0472552 | 9602.9 | 87.3 |
| .480 | .0165507 | 3422.1 | 34.6 | .0482199 | 9690.1 | 86.9 |
| .485 | .0168946 | 3456.7 | 34.6 | .0491932 | 9776.8 | 86.6 |
| .490 | .0172420 | 3491.2 | 34.5 | .0501752 | 9863.2 | 86.2 |
| .495 | .0175929 | 3525.7 | 34.5 | .0511659 | 9949.2 | 85.8 |
| .500 | .0179472 | 3560.2 | 34.5 | .0521651 | 10034.8 | 85.4 |
| .505 | .0183049 | 3594.6 | 34.4 | .0531728 | 10119.9 | 85.0 |
| .510 | .0186661 | 3629.0 | 34.4 | .0541890 | 10204.7 | 84.6 |
| .515 | .0190307 | 3663.4 | 34.3 | .0552137 | 10289.1 | 84.2 |
| .520 | .0193988 | 3697.7 | 34.3 | .0562468 | 10373.1 | 83.8 |
| .525 | .0197703 | 3732.0 | 34.3 | .0572883 | 10456.7 | 83.4 |
| .530 | .0201452 | 3766.3 | 34.2 | .0583382 | 10539.9 | 83.0 |
| .535 | .0205235 | 3800.5 | 34.2 | .0593963 | 10622.7 | 82.6 |
| .540 | .0209053 | 3834.7 | 34.2 | .0604627 | 10705.1 | 82.2 |
| .545 | .0212905 | 3868.8 | 34.1 | .0615373 | 10787.1 | 81.8 |
| .550 | .0216791 | 3903.0 | 34.1 | .0626201 | 10868.6 | 81.4 |
| .555 | .0220711 | 3937.0 | 34.1 | .0637111 | 10949.8 | 81.0 |
| .560 | .0224665 | 3971.1 | 34.0 | .0648101 | 11030.6 | 80.6 |
| .565 | .0228653 | 4005.1 | 34.0 | .0659171 | 11111.0 | 80.2 |
| .570 | .0232675 | 4039.1 | 34.0 | .0670322 | 11190.9 | 79.7 |
| .575 | .0236731 | 4073.0 | 33.9 | .0681553 | 11270.4 | 79.3 |
| .580 | .0240821 | 4106.9 | 33.9 | .0692863 | $1134\overline{9}.5$ | 78.9 |
| .585 | .0244945 | 4140.8 | 33.8 | .0704252 | 11428.3 | 78.5 |
| .590 | .0249103 | 4174.6 | 33.8 | .0715720 | 11506.5 | 78.1 |
| .595 | .0253294 | 4208.4 | 33.8 | .0727265 | 11584.4 | 77.7 |
| .600 | .0257519 | 4242.2 | 33.7 | .0738888 | 11661.9 | 77.3 |



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